

**CMTC-502866-MS**

## **Enhanced Oil Recovery – The History of CO<sub>2</sub> Conventional WAG Injection techniques developed from Lab in the 1950's to 2017**

David Merchant, Merchant Consulting

Copyright 2017, Carbon Management Technology Conference

This paper was prepared for presentation at the Carbon Management Technology Conference held in Houston, Texas, USA, 17–19 July 2017.

This paper was selected for presentation by a CMTC program committee following review of information contained in an abstract submitted by the author(s). Contents of the paper have not been reviewed and are subject to correction by the author(s). The material does not necessarily reflect any position of the Carbon Management Technology Conference, its officers, or members. Electronic reproduction, distribution, or storage of any part of this paper without the written consent of the Carbon Management Technology Conference is prohibited. Permission to reproduce in print is restricted to an abstract of not more than 300 words; illustrations may not be copied. The abstract must contain conspicuous acknowledgment of CMTC copyright.

---

### **Abstract**

During the past 45 years, CO<sub>2</sub> flood technology for Enhanced Oil Recovery projects evolved from a partially understood process filled with uncertainties to a process based on proven technology and experience. Many questions involved with CO<sub>2</sub> flooding have been thoroughly analyzed and answered. This knowledge is currently being used by a limited number of companies that actually know how to design, implement, and manage a CO<sub>2</sub> flood for long term profit. The purpose of this report is to help disseminate this knowledge to operating companies interested in EOR flooding or to CO<sub>2</sub> Sequestration Communities interested in storing CO<sub>2</sub> in EOR projects.

In 2015, Merchant Consulting published CMTC-440075-MS “Life beyond 80 – A look at Conventional WAG Recovery beyond 80% HCPV Injection in CO<sub>2</sub> Tertiary Floods”. The primary objective of the report was to target all 10 CO<sub>2</sub> Recovery Methods used today including “Conventional WAG Techniques” which have been used in over 90% of all the Enhanced Oil Recovery projects implemented to date. These include projects in the Permian Basin in Texas, Colorado, Oklahoma, and Wyoming. The paper presents answers to the question “What is life after 80% HCPV Injected?” And “What effect does life after 80% HCPV have on Tertiary Oil Recovery, CO<sub>2</sub> Utilization and CO<sub>2</sub> Retention in different producing formations?” Results of this study show Tertiary Oil Recovery can be as high as 26% OOIP when slug sizes exceed 190% HCPV injected.

### **Conventional WAG History in CO<sub>2</sub> Tertiary Oil Projects:**

To achieve CO<sub>2</sub> Injection beyond 80% HCPV Injection requires proper CO<sub>2</sub> WAG Management. The purpose of this report is to provide both the EOR and CO<sub>2</sub> Sequestration Communities an understanding of the “History of Conventional WAG” and how it has changed from first introduced in the Lab in the 1950's, to how it was implemented and developed in the 1980's by the Major Oil Companies in the Permian Basin, and how Conventional WAG is being managed today in the field.



# CO<sub>2</sub> Tertiary Recovery Methods

## Introduction

CO<sub>2</sub> Tertiary Recovery Processes to date encompass “**Ten**” Recovery Methods. Four of these methods are used in the Permian Basin. Conventional WAG Techniques have been used in over 90+% of the CO<sub>2</sub> floods around the World. The Seminole field example presented in this report is an example of a field operated under Conventional WAG that targets both the Main Pay and ROZ zones.

### Tertiary CO<sub>2</sub> Flooding

#### Ten CO<sub>2</sub> Recovery Methods used for Tertiary Oil Recovery in the United States

1. Conventional WAG Recovery (90%+)
2. Residual Oil Zone (ROZ) (Seminole)
3. Gravity Drainage (Yates Field)
4. Double Displacement (Yates Field)
5. Gas Cycling (Denbury, Mississippi).
6. Huff-and-Puff (100+ Projects)
7. Heavy Oil - Calif. (14+ API Gravity)
8. Shale Oil (Bakken) (Under Investigation)
9. Horizontal Well Pattern Development
10. CO<sub>2</sub> Gas Drive w/ Nitro Boost

#### Tertiary CO<sub>2</sub> Flooding

##### Ten CO<sub>2</sub> Recovery Methods used for Tertiary Oil Recovery in the United States

1. Conventional WAG Recovery (90%+)
2. Residual Oil Zone (ROZ) (Seminole)
3. Gravity Drainage (Yates Field)
4. Double Displacement (Yates Field)
5. Gas Cycling (Denbury, Mississippi).
6. Huff-and-Puff (100+ Projects)
7. Heavy Oil - Calif. (14+ API Gravity)
8. Shale Oil (Bakken) (Under Investigation)
9. Horizontal Well Pattern Development
10. CO<sub>2</sub> Gas Drive w/ Nitro Boost

#### Tertiary CO<sub>2</sub> Flooding

##### Ten CO<sub>2</sub> Recovery Methods used for Tertiary Oil Recovery in the United States

1. Conventional WAG Recovery (90%+)
2. Residual Oil Zone (ROZ) (Seminole)
3. Gravity Drainage (Yates Field)
4. Double Displacement (Yates Field)
5. Gas Cycling (Denbury, Mississippi).
6. Huff-and-Puff (100+ Projects)
7. Heavy Oil - Calif. (14+ API Gravity)
8. Shale Oil (Bakken) (Under Investigation)
9. Horizontal Well Pattern Development
10. CO<sub>2</sub> Gas Drive w/ Nitro Boost

Additional information can be found: SPE Paper 139516 or CMTC-502866-MS (“Life Beyond 80 – A look at Conventional WAG Recovery beyond 80% HCPV Injection in CO<sub>2</sub> Tertiary Floods”)

## Carbon Sequestration Options: Ten Recovery Methods for EOR

Most Enhanced Oil Recovery Projects use one of the following **ten** operating methods: Conventional WAG Recovery, ROZ Recovery, Gravity-stabilized Recovery, Double Displacement, Gas-cycling Huff-and-Puff, Heavy Oil-California, Shale Oil (Bakken, Wolfcamp), Horizontal Well Pattern Development, and CO<sub>2</sub> Gas Drive w/ Nitro Boost. The primary difference between methods depends on the reservoir geology and well pattern configuration. In Conventional CO<sub>2</sub> floods, typical of West Texas, the formations are basically flat (Ramp Sequence), low perm, the fields are developed on pattern spacing (e.g. 5-spot patterns, 9-spot patterns, or Chickenwire patterns), and Conventional WAG Operating schemes are used to control mobility and CO<sub>2</sub> flood response. In conventional WAG operations, the objective is to minimize the amount of CO<sub>2</sub> purchased (CO<sub>2</sub> stored in Sequestration projects), which is typically in the range of range of 30%-50% of the total HCPV CO<sub>2</sub> injected. In un-conventional Gravity-Stabilized and Double Displacement case histories, Flue Gas, CO<sub>2</sub>, Lean Gas or N<sub>2</sub> is usually injected in the top of the structure and oil is produced from the bottom. More CO<sub>2</sub> can be sequestered than conventional WAG operations. As much as 80% of the total pore volume can be displaced with CO<sub>2</sub>. In Gas-cycling projects, typical of projects operated by Denbury in Mississippi, CO<sub>2</sub> is cycled through the formation. As much as 6 pore-volumes of CO<sub>2</sub> are injected to recover 18% OOIP. In Huff-and-Puff operations, the CO<sub>2</sub> is injected into and produced from the same well. The objective is to mobilize tertiary oil in the near vicinity of the well-bore, and then produce the CO<sub>2</sub> and tertiary oil back. In California the Wilmington field had three CO<sub>2</sub> pilots in 14 API Gravity Crude. Recovery was comparable with West Texas Operations. Shale Oil with CO<sub>2</sub> is still under investigation. Horizontal Well CO<sub>2</sub> floods are operational in Aneth field in Utah and Weyburn field in Canada. The Gravity Drainage case with added Nitro-Boost was developed for rate acceleration cases where nitrogen follows CO<sub>2</sub> Injection.

## CO<sub>2</sub> Storage - Mis-conceptions about EOR

Over the years, there have been many mis-conceptions and half truths developed about EOR and its ability to store CO<sub>2</sub>.

The **first mis-conception** about CO<sub>2</sub> flooding deals with ranges of Tertiary Oil Recovery reported over the years. In the 1990's, most all of the major oil companies reported tertiary oil recovery in the range of 10%-12% OOIP with a 30%-40% HCPV CO<sub>2</sub> slug size. By 2000, this number grew to 18% OOIP recovery with an 80% slug size. Today, expected recoveries in certain fields are expected to exceed 26% OOIP with 190% HCPV CO<sub>2</sub> injected. However, NOT all fields will achieve this level of oil recovery. Each CO<sub>2</sub> project must be judged on its own merits.

The **second mis-conception** about CO<sub>2</sub> flooding deals with the amount of CO<sub>2</sub> Storage in EOR operations. Normal EOR operations have always stored or trapped CO<sub>2</sub> in the reservoir. Tertiary recovery is a displacement process. For the EOR process to work, CO<sub>2</sub> must be cycled through the reservoir, similar to water flood operations. The CO<sub>2</sub> acts as a solvent to swell the remaining oil left after water flood and decreases the oil's viscosity; thus, allowing the tertiary oil to flow. Three phase relative permeability dictates the amount of CO<sub>2</sub> trapped in the formation due to phase trapping. From existing CO<sub>2</sub> flood evaluations, this equates to the amount of CO<sub>2</sub> purchased and represents approximately 30%-40% of the Hydrocarbon-Pore-Volume. With extended WAG with CO<sub>2</sub> volumes exceeding 125% HCPV, the storage capacity could increase to 50%-60% HCPV, but involves large volumes of CO<sub>2</sub> through-put with little incremental gain in oil recovery.

The **third mis-conception** deals with throughput Injection Rate and Injection Pressure (Water Injection or CO<sub>2</sub> Injection). All reservoirs have a Maximum Through-put Rate that can be injected into the reservoir. The maximum amounts of CO<sub>2</sub> that can be stored in a reservoir are based on a number of factors. These include: The total number of production and injection wells available, pattern configuration, current reservoir pressure, fracture pressure, injection flow capacity (permeability-thickness (kh) of each injection well), and relative permeability. Most water flood operations operate at or near fracture pressure. The same is true for CO<sub>2</sub> floods. The objective is to provide maximum CO<sub>2</sub> throughput rate across the reservoir at a level that maintains good seal integrity.

The **fourth mis-conception** about CO<sub>2</sub> flooding deals with the Total CO<sub>2</sub> Storage Capacity of a reservoir. To date, all CO<sub>2</sub> floods operate with the intent to minimize the amount of CO<sub>2</sub> purchased. Under these conditions, CO<sub>2</sub> is purchased up-front and cycled through the reservoir until the revenue from the oil and hc-gas production doesn't have the ability to support the cost to recover the oil (abandonment). This date has been very elusive to determine. Of all the CO<sub>2</sub> projects operated to date, most are still operating today. A limited few projects have been shut-in due to a low oil price environment, but could be returned back to production if given the right economic conditions.

The **fifth mis-conception** about CO<sub>2</sub> flooding deals with CO<sub>2</sub> Storage Timing. Is it at the beginning? Does it occur during EOR CO<sub>2</sub> operations? Or, is it at the end of EOR operations? For those advocating a switch from EOR to CO<sub>2</sub> Storage two-thirds though or near the end of the EOR project should think through the physics. You can't fool Mother Nature. The amount of CO<sub>2</sub> **TRAPPED, STORED, OR SEQUESTERED** is dependent on the Composition of the Residual Oil Saturation and Phase Trapping of the Non-Wetting Phase, which occurs throughout the life of CO<sub>2</sub> injection, with 75% of CO<sub>2</sub> storage occurring during the first one-third of the project's life. After this initial period, most of the CO<sub>2</sub> that is injected is re-cycle CO<sub>2</sub> from the CO<sub>2</sub> recovery plant. CO<sub>2</sub> purchases near the end of the life of an EOR project are minimal.

The **last mis-conception** deals with achieving Total CO<sub>2</sub> Storage Potential of the reservoir. Currently there are ten methods used by the industry to recover oil with CO<sub>2</sub>. All target the remaining tertiary oil. None target the **water**. The Eleventh Recovery Method which targets CO<sub>2</sub> storage removes both the **CO<sub>2</sub>** and **Water** from the reservoir. In a World where there is an infinite amount of CO<sub>2</sub> available for storage, the remaining water in the reservoir becomes a commodity target along with the oil. Under this scenario, the objective will be to displace as much of the remaining **oil plus water** from the reservoir and replace it with CO<sub>2</sub>. Since seal integrity will always be maintained below formation parting fracture pressure, the additional storage capacity provided by removing both the oil and water would far exceed EOR storage operations alone.





# Conventional WAG History

## Lab Experiments in the 1950's and 1960's

Conventional Water-Alternating-Gas (WAG) was originally discovered in the 1950's when Caudle and Dyes introduced water in Lab experiments to decrease gas mobility. During the 1960's over 150 small scale Miscible and Immiscible projects were implement across the United States by labs and oil companies interested in developing Enhanced Oil Recovery for additional recovery of oil beyond Waterflood operations.

**Permian and Rocky Mountain Basins  
History of "WAG"**

**1950's and 1960's**  
 1950's - 150 Small Scale Miscible and Immiscible Projects  
 1958 - Lab Experiments Caudle and Dyes introduced water to decrease solvent mobility

**1970's**  
 1972 - Sacroc Unit (Kelly Snyder field) First Commercial Large Scale Project  
 1972-1979 North Cross, Two Freds, Maljamar, others

**1980's Large Scale Permian Basin and Rocky Mountain Expansions**  
 Slaughter field three projects plus Wasson ODC Unit - Amoco's Tapered WAG  
 Wasson field Denver Unit - Shell's Continuous Injection area plus DUWAG  
 Wasson field Willard Unit - Arco's Area Wide WAG went to Individual Patterns  
 Seminole field - Amerada Hess's Constant WAG scheme  
 Rangely field - Chevron's Wide Area WAG scheme  
 Bairoil (Lost Soldier and Wertz field ) - Amoco's Tapered WAG

**1990's, 2000's, and 2010's**  
 Most new CO<sub>2</sub> flood projects adopt the "Tapered WAG" approach to WAG Management

**SPE 18977 (1989), Table 1**

Field	State	Reservoir	Lithology	%HCPV Injected	Rec Eff, % OOIP	Gross Utilization, Mcf/Bbl	Net Utilization, Mcf/Bbl
<b>Field Scale</b>							
Dollarhide	Texas	Devonian	Trip Chert	30	14		2.4
East Vacuum	Texas	San Andres	Oolitic Dolomite	30	8	11.1	6.3
Ford Geraldine	Texas	Delaware	Sandstone	30	17	9	5
Means	Texas	San Andres	Dolomite	55	7.1	15.2	11
North Cross	Texas	Devonian	Trip Chert	40	22	18	7.8
Northeast Purdy	Oklahoma	Springer	Sandstone	30	7.5	6.5	4.6
Rangely	Colorado	Weber	Sandstone	30	7.5	9.2	5
Sacroc (17 Pattern)	Texas	Canyon Reef	Carbonate	30	7.5	9.7	6.5
Sacroc (4 Pattern)	Texas	Canyon Reef	Carbonate	30	9.8	9.5	3.2
South Welch	Texas	San Andres	Dolomite	25	7.6		
Two Freds	Texas	Delaware	Sandstone	40	15.6	15.6	8
Wertz	Wyoming	Tensleep	Sandstone	60	10	13	10

SPE 18977 Brock and Bryon 1989

## CO<sub>2</sub> Flooding in 1970's

### First Commercial Scale CO<sub>2</sub> Flooding in 1970's

Chevron, who operated the Sacroc Unit in the Permian Basin, was the first field to inject CO<sub>2</sub> as a commercial project in 1972. Chevron injected CO<sub>2</sub> over the total unit with less than 15% in any one pattern and sold the property in 1992 to Pennzoil. Pennzoil ramped up CO<sub>2</sub> Injection and implemented a 300 acre pilot in the middle of the field of which 1/3 of the total field's production out of 55,000 acres was being produced from the pilot area. In 1998, Pennzoil sold the field to Devon and Devon then sold the field to Kinder Morgan in 2000. Kinder Morgan then ramped-up CO<sub>2</sub> injection to over 900 MMSCFIPD. The result was a Tertiary oil response growth from 9,600 BOPD to over 30,000 BOPD.

**Permian Basin - 1970's to 2017**  
**"First Commercial CO<sub>2</sub> Flood - 1972"**  
**Sacroc Unit in Kelly Snyder Field**

**EXISTING MARKETS**  
Year 2000

**CURRENT CO<sub>2</sub> SOURCES and PIPELINES**

Wyoming Canadian

Sacroc Unit Kelly Snyder Field

Permian Basin Louisiana/Mississippi

**Sacroc Unit - Historical Performance**

Chevron Ownership Pennzoil Operatorship

First Commercial CO<sub>2</sub> flood in 1972 1992 - 1999

Kinder Morgan Operatorship 2000 to Present

Devon Operatorship 1999 - 2000

Waterflood Injection Startup - 1955 Waterflood Injection Expansion CO<sub>2</sub> Startup - 1972

Over the course of CO<sub>2</sub> Tertiary History, the Sacroc Unit has had several operators over time

Chevron should be commended for implementing the first Commercial CO<sub>2</sub> flood in 1972

Pennzoil and Devon operated in the 1990's, but lacked the capital to make large scale investments

Kinder Morgan which in 2003 ramped up CO<sub>2</sub> Purchases bringing oil production to 30,000 BOPD in 2017

**The Kelly Snyder Field (Sacroc Unit) recovers Tertiary Oil from the Canyon Reef Limestone Formation about 6,700 ft. deep**

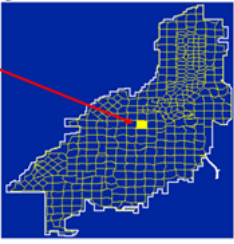
- Date of Discovery: November, 1948
- Total Acreage: 55,000 acres
- Original Oil-in-place: 2.88 Billion stb
- Total Wells: 5,020 wells
- Field Utilization: March, 1953
- Water Injection: September, 1954
- CO<sub>2</sub> Flooding: January, 1972

Chevron should be commended for implementing the first Commercial CO<sub>2</sub> flood in the United States, but only sprinkled CO<sub>2</sub> over the total reservoir limit.

## Sacroc Unit – Historical Performance

### Pennzoil Operatorship (1992-1998)

**Sacroc Unit – Pennzoil Ownership**  
Center-line Project

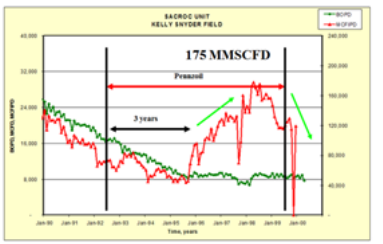


1996 CO<sub>2</sub> Pattern Development Plan 300 Acre Pilot

**Pennzoil Team**

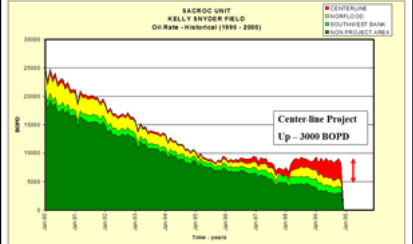
1. Dr. Ghasem Bayat
2. Tony Bevegeau
3. Claud Pickard
4. Jack Horkowitz
5. Tom Wiggate
6. Don Hartman

**Sacroc Unit – Pennzoil Ownership**  
Historical Production – Oil Production and CO<sub>2</sub> Injection



175 MMSCFD

**Sacroc Unit – Pennzoil Ownership**  
Historical Production by Project Area



Center Line Project Up - 2000 BOPD

Chevron should be commended for being the first Commercial CO<sub>2</sub> flood, but over the course of time sprinkled CO<sub>2</sub> into the Reservoir.

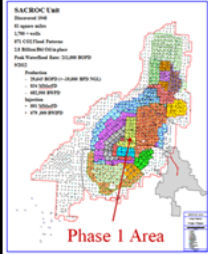
Pennzoil implemented a 300 acre Centerline Pilot Project in 1996 which produced 1/3 of the total field's production over the total 55,000 acre unit boundary

Pennzoil in 1996 implemented a 300 acre Centerline Pilot Project which produced one third of the fields 9,600 BOPD production. (Ref: 106) In 1998, Pennzoil sold the field to Devon who later sold the field to Kinder Morgan in 2000.

## Sacroc Unit – Historical Performance

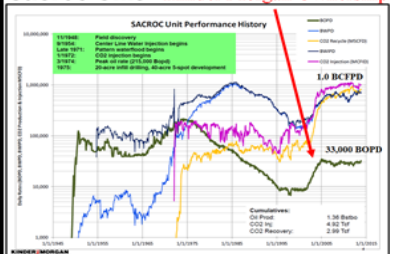
### Kinder Morgan Operatorship (2000 -Present)

**SACROC Unit Reservoir Management**



Phase 1 Area

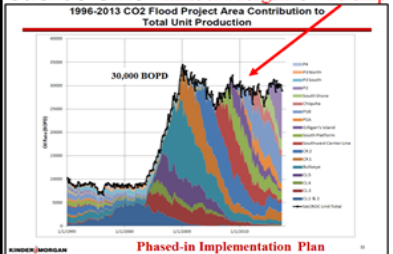
**Sacroc Unit – Kinder Morgan Ownership**  
SACROC Unit Performance History



1.0 BCFPD

33,000 BOPD

**Sacroc Unit – Kinder Morgan Ownership**  
1996-2013 CO<sub>2</sub> Flood Project Area Contribution to Total Unit Production



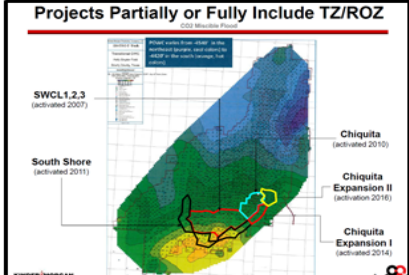
30,000 BOPD

Phased-in Implementation Plan

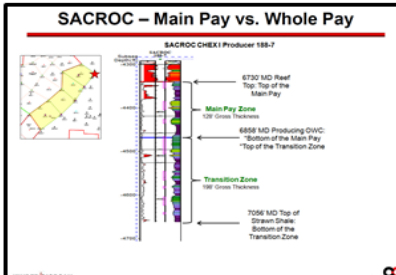
Kinder Morgan implemented a phased-in Tertiary Development Plan and expanded CO<sub>2</sub> Injection to over 1,000 MMSCFIPD which resulted in a 30,000 BOPD Response still seen in 2017. WAG Management is on an Individual Pattern Basis with Multiple Pattern Development programs developed over time

**ROZ Pay Zone**

Projects Partially or Fully Include TZ/ROZ



**SACROC – Main Pay vs. Whole Pay**



6730 MD Reef Top, Top of the Main Pay

Main Pay Zone 128 Green Thickness

6658 MD Producing OWC Bottom of the Main Pay Top of the Transition Zone

Transition Zone 196 Green Thickness

7056 MD Top of Stream Drain Bottom of the Transition Zone

**Conclusions**

- TZ/ROZ is highly responsive to miscible CO<sub>2</sub> flooding
- TZ/ROZ not targeted in primary and secondary recovery
- TZ/ROZ oil saturation similar to or better than main pay after water flooding
- Multiple TZ/ROZ projects now have repeatedly shown favorable performance
- Even in areas with long production histories there is still potential to find more

Kinder Morgan has also targeted the Residual Oil Zone below the Main Pay Zone. Multiple TZ/ROZ projects have repeatedly shown favorable performance

In 2000, Kinder Morgan implemented a multi-phase Tertiary Development Plan that increased CO<sub>2</sub> Injection to over 800 MMSCFIPD, which resulted in a 30,000 BOPD Response still seen in 2017.



# CO<sub>2</sub> Flooding in 1980's

In the 1980's, major oil companies including Shell, Amoco, Texaco, Arco, Phillips, Oxy, and Exxon implemented CO<sub>2</sub> projects in many of the large fields located across the Permian Basin, Rockies, and Gulf Coast Regions. As reported by the major oil companies, expected tertiary recovery was typically in the 8% to 12% OOIP range. Optimum slug size for most projects was projected to be in the 30% to 40% HCPV CO<sub>2</sub> injection range.

**1980's Permian Basin - Slaughter Estate Unit**

**Amoco's Tapered WAG Management (SPE 26624)**

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

**Example - WAG BENEFITS (Controlled CO<sub>2</sub> Process)**  
Permian Basin - Slaughter Estate Unit in Slaughter Field

In 1989, Amoco converted from Constant WAG to Tapered WAG Management which provided the means to "Level Load" gas production to the Plant Inlet Gas Rate thus allowing control over the CO<sub>2</sub> Process.

**1980's Tertiary CO<sub>2</sub> Flooding Permian Basin (Wasson Field)**

**Wasson Field Location**

**Wasson Field**

**Wasson Field**

The Wasson field recovers Tertiary Oil from the San Andres Formation about 5,500 ft. deep from various leases and operators located across this large field and contains a large Residual Oil Zone (ROZ).

**Tertiary CO<sub>2</sub> Flooding Permian Basin (Seminole Field)**

**Seminole Field Location**

**Seminole Field**

**Seminole Field**

The Seminole field recovers Tertiary Oil from the San Andres Formation about 5,500 ft. deep which also includes a large Residual Oil Zone (ROZ). The Field is developed on 9-spot pattern spacing.

**Rocky Mountain Region**

**Rangely Weber Unit - (Colorado) Comparison**

**Bairoil Field - Lost Soldier and Wertz (Wyoming)**

**Lost Soldier - Structure Maps**

**On the Outside they both look the same**

In the 1980's, Major Oil Companies also implemented different types of CO<sub>2</sub> Recovery Methods to both experiment and determine which process works best. Each will be discussed below.

**Permian and Rocky Mountain Basins History of "WAG"**

**1980's Large Scale Permian Basin and Rocky Mountain Expansions**

- Slaughter field three projects plus Wasson ODC Unit – Amoco's Tapered WAG
- Wasson field Denver Unit – Shell's Continuous Injection area plus DUWAG
- Wasson field Willard Unit - Arco's Area Wide WAG went to Individual Patterns
- Seminole field – Amerada Hess's Constant WAG scheme
- Rangely field – Chevron's Wide Area WAG scheme
- Bairoil (Lost Soldier and Wertz field ) – Amoco's Tapered WAG



## CO<sub>2</sub> Flooding in 1980's (Amoco – Tapered WAG)

Amoco initiated CO<sub>2</sub> injection into four floods in the mid 1980's. These included: Slaughter Estate Unit, Central Mallet Unit, and Frazier Unit in Slaughter field plus Wasson ODC in Wasson field. All initially were operated under a constant WAG. During this time frame, extensive modelling was conducted to determine a method that could optimize the WAG process and extend oil recovery. (Ref: 107) The result was “Tapered WAG” which provided the means to “Level Load” total gas production from the field to a maximum “Plant Inlet Gas Rate”. In 1989, Amoco implemented this new technology into all four projects, achieving total success.

As this technology improved, advancements in CO<sub>2</sub> flood design have been implemented into more improved reservoir management practices. In the 1990's, Constant WAG was being replaced with Tapered WAG operations and tertiary oil recovery increased to 18% of a field's Original Oil-in-Place. Today, most fields implemented during the 1980's have surpassed the 40% HCPV injection, advancing to or passing earlier HCPV CO<sub>2</sub> predictions.

**Amoco's Tapered WAG Management – 1980's**

**Slaughter Estate Unit - Example**

**Conventional WAG Injection Techniques**

**Definitions WAG Process**

**Pattern Parameters**

CO<sub>2</sub> Tertiary floods are designed to operate best in fields that have been drilled on 5-spot, 9-spot, or Chicken-wire development patterns

**Amoco Tertiary Performance – 1980's**

**Tapered WAG Injection**

**Reservoir Simulation**

SPE Paper 26624 - Reservoir Management in Tertiary CO<sub>2</sub> Floods

Reservoir Management utilizing Amoco's Tapered WAG approach provided the ability to “Level Load” gas production in 1989

**Amoco WAG Management – 1980's**

**Tapered WAG Injection**

SPE Paper 26624 - Reservoir Management in Tertiary CO<sub>2</sub> Floods

**Production Montage** **Pattern Montage** **Integrated Montage**

An Integrated approach to Reservoir Management was a vital tool in understanding the WAG Process in the 1980's

**1980's**

**Example - WAG BENEFITS (Control CO<sub>2</sub> Process)**

**Permian Basin - Slaughter Estate Unit in Slaughter Field Production and Injection (1984 – 1994)**

Amoco Team: Kevin McCullough, Steve Paschal, Bart Nelson, John Kishelberg, David Merchant

The WAG increase in 1989 “Level Loaded” gas production to the Plant Inlet Rate, which provided the ability to control gas production throughout the life of the flood, thus advancing CO<sub>2</sub> tertiary recovery beyond the 8% to 12% OIIP documented in most studies.

**1980's**

**Example - WAG BENEFITS (Control CO<sub>2</sub> Process)**

**Level Load Gas Production WAG Change - 1989**

Amoco's Tapered WAG Management provided the means to “Level Load” gas production to the Plant Inlet Rate, but “Over-WAGGED” causing the gas production to be less than inlet rate. To compensate Amoco then initiated individual pattern WAG adjustments to better fine tune gas production back to plant inlet rate

**Reservoir Simulation**

**Reservoir Model Study - San Andres 5 Spot**

Single 5 Spot Pattern (10X10X6 Grid)

**Injection Profiles**

**X-Cross Section - Oil Saturation**

Reservoir Simulation was a vital tool in understanding the WAG Process in the 1980's

**Reservoir Simulation**

**Continuous** **Constant WAG** **Tapered WAG**

**Injection Profiles – 20% HCPV to 70% HCPV**

Tapered WAG provides Mobility Control in the Fast Zones to “Level Load” gas production to the Plant Inlet Gas Rate

Slaughter Field Bibliography References: 19 thru 29

“Tapered WAG Management” can provide Reservoir Engineers with a “Reservoir Management Tool” that can properly manage WAG, but only through proper “Reservoir Management Practices”

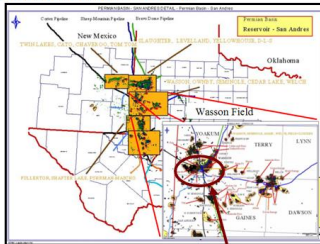
## CO<sub>2</sub> Flooding in 1980's Wasson Field (Shell, Arco, and Amoco)

Shell, in the Denver Unit of Wasson field took a different approach to understanding CO<sub>2</sub> management. It first divided the Denver Unit up into three project areas. The main area was a Continuous Injection project where they targeted 4% HCPV/per year, the second project area was a Constant WAG injection area (DUWAG Area) where they targeted 2% HCPV/per year CO<sub>2</sub> and 2% HCPV/per year Water. The final injection area in the western part of the unit was poorer quality reservoir and remnants of a gas cap. As technology improved, advancements in CO<sub>2</sub> flood design were implemented into reservoir management practices by Shell through the 1990's. The nine-spot inverted line drive configuration was changed to more of a direct line drive after conformance issues were identified in the field based on performance and pattern adjustments could better control conformance issues.

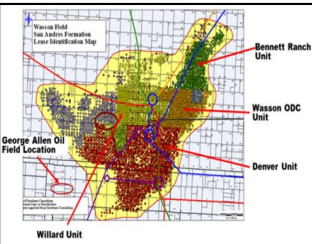
### 1980's Tertiary CO<sub>2</sub> Flooding

#### Permian Basin (Wasson Field)

**Wasson Field Location**



**Wasson Field**



**Wasson Field**

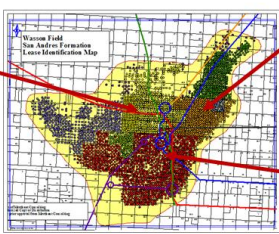
The Wasson field recovers Tertiary Oil from the San Andres Formation about 5,500 ft. deep from various leases and operators located across this large field and contains a large Residual Oil Zone (ROZ).

Arco, in the Willard Unit first implemented an area wide switching program based on making large area switches. The reservoir responded with some injectors taking 4% HCPV where others may have had 1% HCPV injected. Due to pattern imbalance issues, Arco then switched to an individual pattern WAG management program.

### 1980's Tertiary CO<sub>2</sub> Flooding

#### Permian Basin (Wasson Field)

**Willard Unit  
(Arco)**



**Wasson ODC Unit  
(Amoco)**

**Denver Unit  
(Shell)**

The Denver Unit, operate by Shell, initiated a Continuous Injection Area targeting 4% CO<sub>2</sub> HCPV/year and a WAG Injection area (DUWAG) where they operated 2% HCPV/year CO<sub>2</sub> and 2% HCPV/year. The Continuous Area was converted to a Line Drive due to conformance orientation issues.

The Wasson ODC Unit, operated by Amoco initiated a WAG down with Amoco's "Tapered WAG" operating scheme in 1989 to "Level Load" gas to the plant inlet rate.

The Willard Unit, operated by Arco initiated early on Large Area Pattern Switches, but later changed to an individual pattern approach.

**Wasson Field**  
Bibliography References:  
7,8,9,10,11,18,12,13,14,15,16

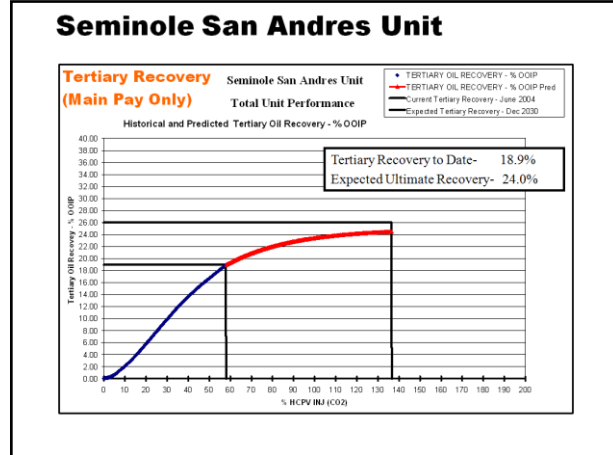
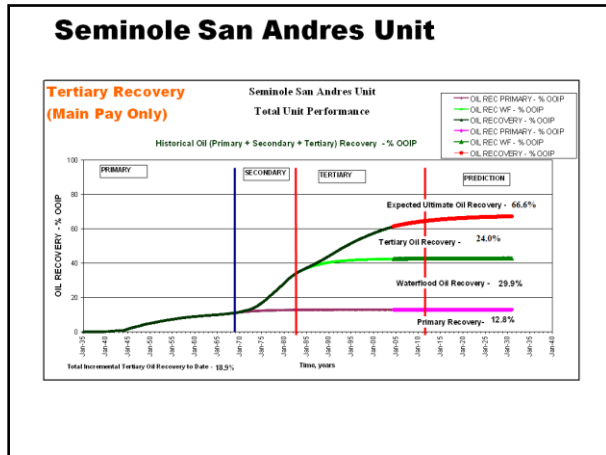
Amoco, in 1989, at the same they implemented Tapered WAG in Slaughter field, implemented a Tapered WAG at Wasson ODC Unit to "Level Load" gas production to its Ryan Holmes Plant Gas Rate Limit. As a result, the benefit of modifying to a Tapered WAG extended Tertiary Oil Recovery way beyond all of Amoco's original model predictions.





### Seminole San Andres Unit – (Main Pay Oil Zone Example)

Primary, Secondary, and CO<sub>2</sub> Tertiary Main Pay Oil Recovery as a percent of Original Oil-in-Place (OOIP) are shown below. Under Primary Operations, the field would have recovered 12.8% of its OOIP before abandoning operations. Water flood operations would have increased oil recovery to 42.7% OOIP (Primary plus Secondary). Tertiary operations with CO<sub>2</sub> in the Main Pay zone would have increased oil production by 24% OOIP. Total Primary+Secondary+Tertiary (MP) = 66.6% OOIP.

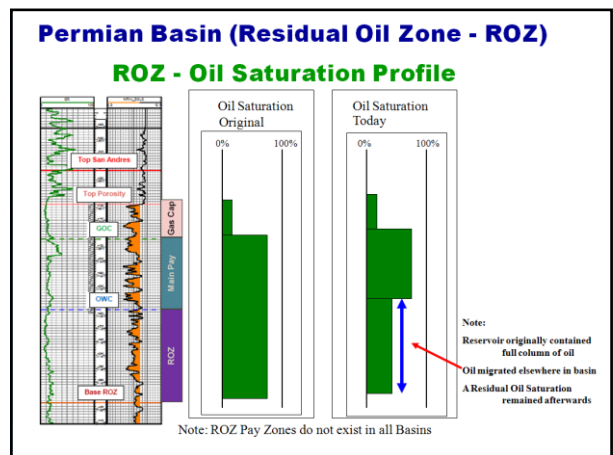
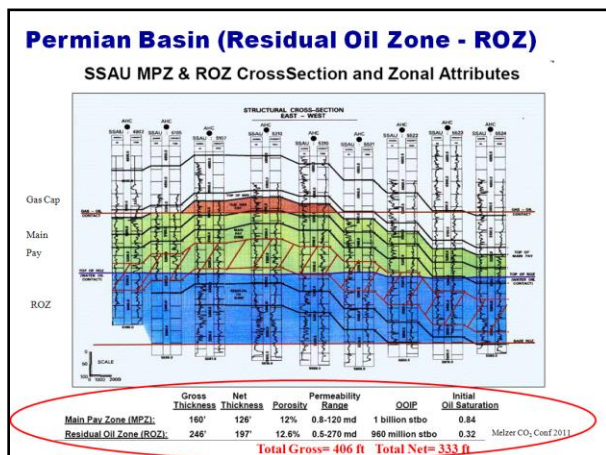


### Seminole San Andres Unit – (Main Pay – Amerada Hess WAG Management)

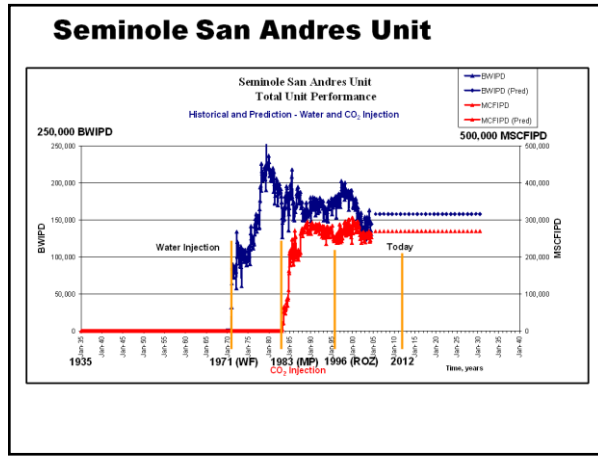
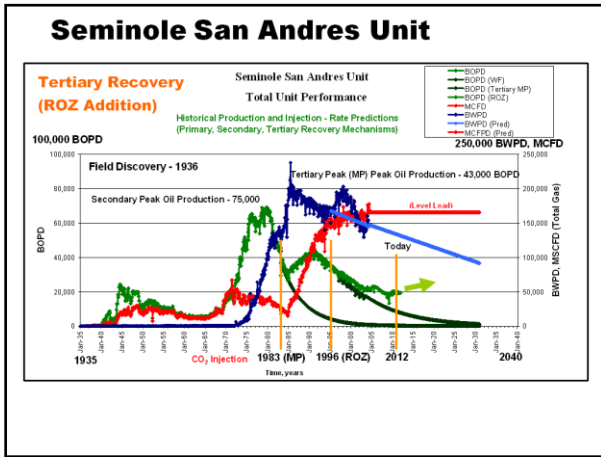
The Main Pay Zone was developed on Inverted a Nine-spot Pattern development. In 1983, the field initiated CO<sub>2</sub> injection into a phased-in pattern development across the field. By 1987, 95% of the CO<sub>2</sub> flood had been completed south to the town of Seminole. Amerada Hess’s WAG Management was based on a 2:1 WAG Ratio with 3.0% HCPV CO<sub>2</sub> Half cycles and 6.0% HCPV Water Half Cycle. The field has maintained or increased the water to better control gas breakthrough over time.

### Seminole San Andres Unit – (Residual Oil Zone (ROZ) Example)

A Residual Oil Zone (ROZ) is created when oil within the original oil column migrates away from the field over geologic time creating a ROZ interval. In addition to the Main Pay Zone, the Seminole field contains a very large Residual Oil Zone (ROZ). The size of the ROZ is about the same size at the residual oil remaining in the Main Pay. CO<sub>2</sub> Injection commenced in 1996 into the ROZ. Injection into the ROZ will extend field life beyond the 2050’s.



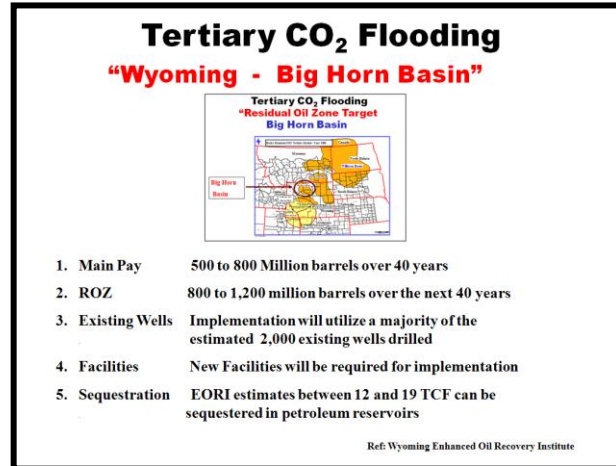
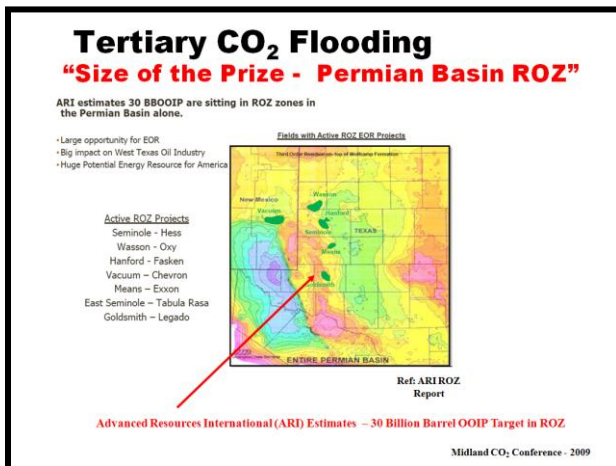
Seminole Unit  
Bibliography References: 58 thru 65



The Residual Oil Zone is responding well to CO<sub>2</sub> Injection. Since the ROZ reserves have never been tied to any Basin Study Estimates, these reserves are “NEW” bookable reserves. Future Performance is based on ROZ reservoir characterization unique to the Seminole field. Tertiary Performance is expected to be similar to that of the Main Pay or better, which depends on the quality of the ROZ pay section.

### Residual Oil Zone (ROZ) Enhanced Oil Recovery Potential

Compared to other types of oil recovery mechanisms, CO<sub>2</sub> is the best method designed to recover tertiary oil from Residual Oil (ROZ) Zones. Residual Oil Zones have been identified across the World. The Permian basin is the first region to identify it, characterize it, and now exploit it. Advanced Resources International has estimated the ROZ in the Permian Basin could contain as much as 30 Billion barrels of recoverable tertiary oil from the ROZ. The Wyoming Enhanced Oil Recovery Institute has estimated the state of Wyoming may contain as much as 800 to 1,200 million barrels of ROZ potential in the Big Horn Basin of Wyoming, not counting potential in other basins in the region.



Anthropogenic CO<sub>2</sub> through CO<sub>2</sub> sequestration could expand this target to areas of the World that contain ROZ zones, but lacked the CO<sub>2</sub> to make the projects economically attractive.

# CO<sub>2</sub> Flooding in the 2000's (New Millennium)

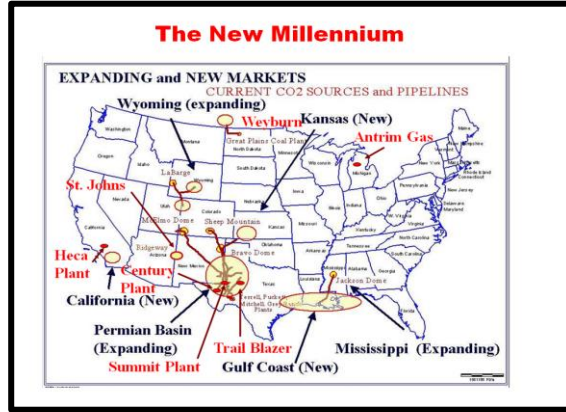
In the 21<sup>st</sup> Century, the benefit of controlling the CO<sub>2</sub> WAG process has extended oil recovery to new levels. As previously shown, the Seminole Main Pay CO<sub>2</sub> flood in the Permian Basin is expected to recover 24% of its Original Oil-in-Place with a 140% HCPV injection of CO<sub>2</sub>, not counting the additional recovery from the ROZ.

**Tertiary CO<sub>2</sub> Flooding**

**“The New Millennium”**

**21<sup>st</sup> Century (2000 and beyond)**

**“Life beyond 80% HCPV Injected”**



However, not all CO<sub>2</sub> floods are alike; Tertiary Oil Recovery from sandstone reservoirs are different from recovery from carbonate reefs just as un-fractured reservoirs are different from fractured reservoirs.

**Tertiary CO<sub>2</sub> Flooding Permian Basin (Seminole Field)**

**Main Pay Performance**

**ROZ Performance**

**ROZ 30 Billion OOIIP Barrel Target**

Since CO<sub>2</sub> Startup in 1983 Tertiary Oil Recovery in the Main Pay is expected to recover 24% OOIP

Since ROZ CO<sub>2</sub> Startup in 1996 Tertiary Oil Response had been excellent with expected ROZ Tertiary Oil Recovery comparable or better than Main Pay Tertiary Oil Recovery

**Tertiary Oil Recovery %OOIP Rec versus %HCPV Inj**

**Un-fractured Sandstone versus Dolomite**

**Permian Basin Dolomite Limestone versus Oklahoma Un-fractured Sandstone Recovery**

**Seminole Field**

**Homogeneous Dolomite - Seminole Unit**

**Uniform**

**Fractured Sandstone versus Dolomite**

**Permian Basin Dolomite Limestone versus Wyoming Tertiary Fractured Sandstone**

**Non-Uniform Pattern Sandstone - Postle field**

**Complex but Understandable**

**Not all Patterns and Reservoirs are alike**

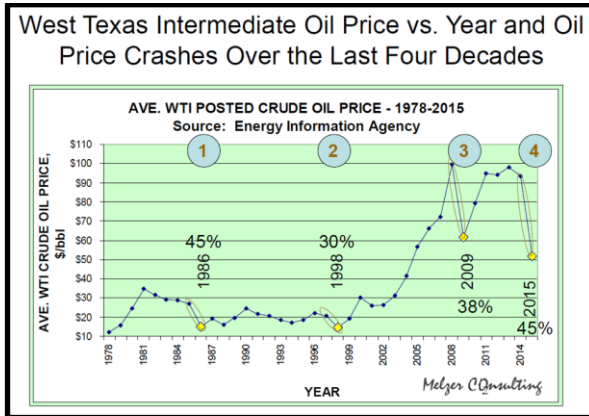
**What are they doing?**

**CO<sub>2</sub> Tertiary Flood Management**

Pattern Review In Progress: Control Central

- WAG management and surveillance systems in place
- 24 hour allocation
- Skilled and professional operators
- Engineering and field personnel participation (and getting it)

- Evaluating Individual Well Performance
- Evaluating Individual Pattern Performance
- Making WAG Adjustments based on Pattern Performance



Ref. 108

Tertiary Oil Recovery with CO<sub>2</sub> has also weathered **Four** Oil Price Adjustment Periods with the last one in 2015 dropping 45% just like the one back in 1986 that also dropped oil price by 45%. Today, over 90% of the CO<sub>2</sub> Floods that were put on in the 1980's are still producing today. This could only be accomplished through **good Reservoir Management Practices** including the “**Pattern Review Process**” where WAG adjustments are made.

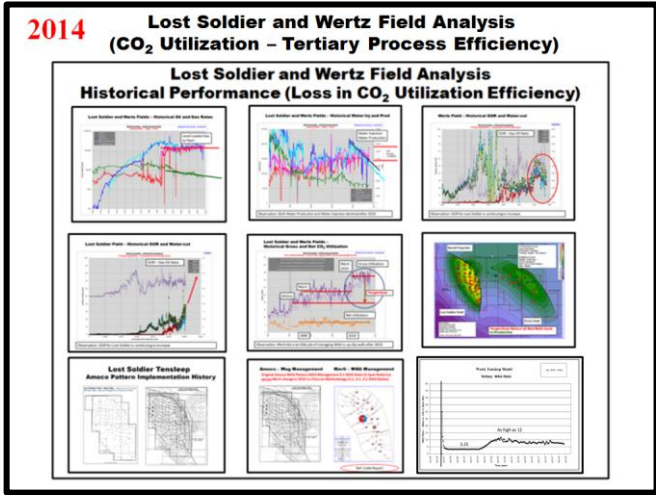
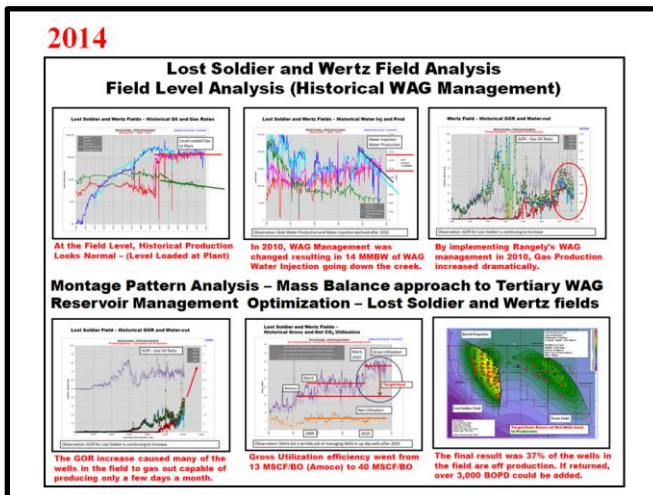
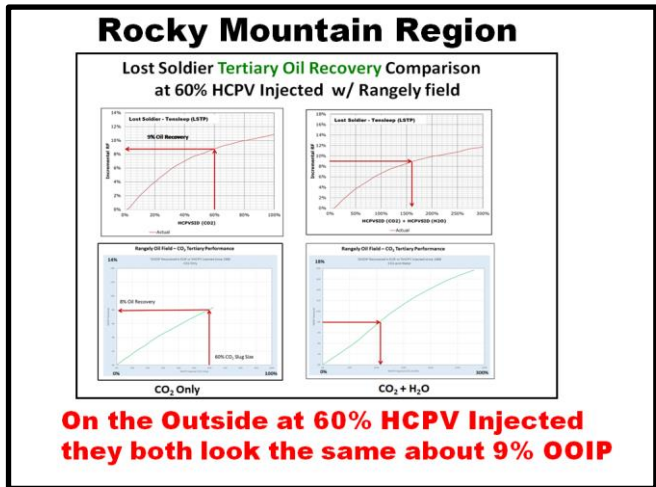
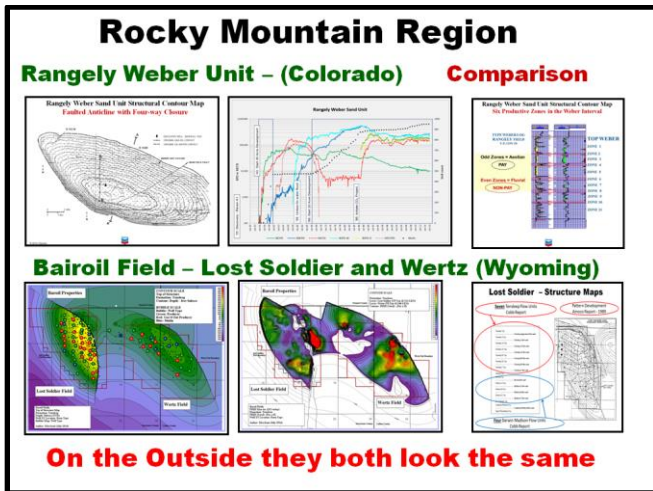


**CO<sub>2</sub> Flooding in the Rocky Mountains (WAG Management Decisions (The Good, the Bad, and the Ugly))**

Different Operators in the 1980’s developed different WAG philosophies depending on the reservoir pattern configuration, formation dip, reservoir pressure, miscibility pressure, etc. As technology improved, advancements in CO<sub>2</sub> flood design were implemented into reservoir management practices to improve overall performance. However, companies should be aware that **NOT** all reservoirs are alike even though they were formed in the same geologic time period with similar producing characteristics.

The example shown below illustrates the fact that not all reservoirs are alike. The Rangely Weber Unit in Wyoming produces from the Weber Sand which is similar in geologic age to Bairoil’s Tensleep Reservoir producing section. In addition, CO<sub>2</sub> Tertiary WAG performance at 60% CO<sub>2</sub> HCPV Injected recovers about 9% OOIIP in both fields.

**NOT ALL FORMATIONS ARE THE SAME**



In 2010, Merit Company, who operated the field, modified Amoco’s five-spot pattern 9:1 WAG scheme to Rangely’s 1:1, 2:1, and 3:1 WAG scheme by dividing the unit up into thirds. From 2010 to 2014, 14 million barrels of water went down the creek that was supposed to be used for WAG Management. The overall effect gassed out 37% of the wells in the Lost Soldier field that deteriorated Amoco’s Gross CO<sub>2</sub> Utilization WAG efficiency rating of 13 MSCF/BO to over 40 MSCF/BO under Merit’s operatorship.

Fortunately **BAD WAG** Practices can be fixed.....

# Life beyond 80% HCPV- (Tertiary Oil Recovery, CO<sub>2</sub> Gross and Net Utilization)

Since 1972, over 130+ Commercial CO<sub>2</sub> floods have been operated in the United States with the majority of these projects still active today. During this time, Engineers have reported a wide range of Tertiary Oil Recovery, Gross Utilization and Net Utilization values at varying stages of maturity. The question becomes “What would Operators report on these CO<sub>2</sub> floods today?” And “What would Oil Recovery, Gross Utilization and Net Utilization look like under Extended CO<sub>2</sub> Slug volumes?” The answer to those questions depends on Reservoir Type. Data from these CO<sub>2</sub> projects from various SPE and DOE reports are listed below by formation type:

**Table 2. - San Andres and Grayburg Formation – Dolomite**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Texas	San Andres	Wasson	Denver Unit	15 to 20	10 to 15	5 to 10	20 to 25	5 to 10	1 to 5	7,8,9,10
Texas	San Andres	Wasson	Denver Unit-ROZ	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	11,18
Texas	San Andres	Wasson	Wasson ODC Unit	15 to 20	10 to 15	5 to 10	20 to 25	5 to 10	1 to 5	12
Texas	San Andres	Wasson	Cornell Unit	15 to 20	10 to 15	5 to 10	20 to 25	5 to 10	1 to 5	13
Texas	San Andres	Wasson	Bennett Ranch Unit	15 to 20	10 to 15	5 to 10	20 to 25	5 to 10	1 to 5	14,15
Texas	San Andres	Wasson	Willard Unit	15 to 20	10 to 15	5 to 10	20 to 25	5 to 10	1 to 5	16
Texas	San Andres	Seminole	Seminole Unit-Main Pay	20 to 25	10 to 15	5 to 10	25 to 30	5 to 10	1 to 5	17
Texas	San Andres	Seminole	Seminole Unit-ROZ	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	11,18
Texas	San Andres	Slaughter	Slaughter Estate Unit	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	19 thru 24
Texas	San Andres	Slaughter	Frazier Unit	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	
Texas	San Andres	Slaughter	Central Mallet Unit	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	25
Texas	San Andres	Slaughter	Slaughter Sundown	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	26, 27,28
Texas	San Andres	Slaughter	Mobil Mallet Unit	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	29
Texas	San Andres	Slaughter	H T Boyd Unit	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	
Texas	San Andres	Slaughter	Igoe Smith	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	
Texas	San Andres	Slaughter	Alex Slaughter Estate	15 to 20	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	
Texas	San Andres	Levelland	Levelland	5 to 10	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	30,31,32
Texas	San Andres	Means (San Andres)	Means (San Andres)	10 to 15	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	33,34
Texas	San Andres	Goldsmith	Goldsmith	10 to 15	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	35,36
Texas	San Andres	Hanford	Hanford	10 to 15	15 to 20	5 to 10	20 to 25	10 to 15	5 to 10	37
New Mexico	Grayburg San Andres	Vacuum	East Vacuum	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	38,39
New Mexico	Grayburg San Andres	Vacuum	Central Vacuum	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	40
New Mexico	Grayburg San Andres	Maljamar	Maljamar Unit	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	41,42
New Mexico	Grayburg San Andres	North Hobbs	North Hobbs	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	
Texas	San Andres	East Penwell (SA) Unit	East Penwell (SA) Unit	5 to 10	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	
Texas	Grayburg	Mabee	Mabee	10 to 15	15 to 20	5 to 10	15 to 20	10 to 15	5 to 10	43
Texas	San Andres	GMK South	GMK South	5 to 10	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	44
Texas	San Andres	Adair San Andres Unit	Adair San Andres Unit	5 to 10	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	
Texas	San Andres	Cedar Lake	Cedar Lake	5 to 10	15 to 20	5 to 10	5 to 10	15 to 20	5 to 10	
Texas	San Andres	Welch	West Welch	5 to 10	15 to 20	5 to 10	10 to 15	10 to 15	5 to 10	45
Texas	San Andres	Welch	South Welch	5 to 10	15 to 20	5 to 10	10 to 15	10 to 15	5 to 10	46
Texas	Grayburg San Andres	Cowden	North Cowden Demo.	5 to 10	15 to 20	5 to 10	5 to 10	15 to 20	5 to 10	
Texas	San Andres	Cowden	South Cowden	5 to 10	15 to 20	5 to 10	5 to 10	15 to 20	5 to 10	47, 48

**Table 3. - Clearfork Formation – Limestone (Tight - Low Permeability)**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Texas	Clearfork	Anton Irish	Anton Irish	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	49
Texas	Clearfork	Wasson (South)	Wasson (South)	1 to 5	10 to 15	5 to 10	1 to 5	10 to 15	5 to 10	50

**Table 4. - Devonian Formation – Tripolitic Chert**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Texas	Devonian	Dollarhide	Dollarhide Devonian Unit	10 to 15	5 to 10	1 to 5	15 to 20	5 to 10	1 to 5	51 thru 54
New Mexico	Devonian	Dollarhide	West Dollarhide Unit	10 to 15	5 to 10	1 to 5	15 to 20	5 to 10	1 to 5	
Texas	Devonian	Dollarhide	North Dollarhide Unit	5 to 10	5 to 10	1 to 5	10 to 15	5 to 10	1 to 5	55
Texas	Devonian	North Cross	N. Cross-Devonian Unit	35 to 40	5 to 10	1 to 5	40 to 45	5 to 10	1 to 5	56-57

**Table 5. - Canyon Reef Formation – Karsted Limestone (High Permeability)**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Texas	Canyon Reef	Kelly Snyder (Sacroc)	Sacroc Unit	10 to 15	10 to 15	5 to 10	15 to 20	10 to 15	5 to 10	58 thru 65
Texas	Canyon Reef	Salt Creek	Salt Creek	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	66,67
Texas	Canyon Reef	Sharon Ridge	Sharon Ridge	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	68
Texas	Canyon Reef	Cogdell	Cogdell	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	69

**Table 6. - Strawn, Morrow, Delaware, Springer, Marmaton, and Yates (Fluivial Deltaic, Point Bar, Turbidite)**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Texas	Strawn	Katz	Katz	10 to 15	10 to 15	5 to 10	15 to 20	10 to 15	5 to 10	70
Oklahoma	Morrow	Postle	Postle	10 to 15	10 to 15	5 to 10	15 to 20	10 to 15	1 to 5	71,72
Oklahoma	Morrow	Camrick	Camrick	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	
Texas	Delaware Ramsey	Twofreds	Twofreds	10 to 15	10 to 15	5 to 10	15 to 20	10 to 15	5 to 10	73,74,75
Texas	Delaware Ramsey	Ford Geraldine	Ford Geraldine	10 to 15	10 to 15	5 to 10	15 to 20	10 to 15	5 to 10	76,77
Texas	Delaware Ramsey	El Mar	El Mar	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	
Texas	Delaware Ramsey	East Ford	East Ford	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	
Texas	Springer	Northeast Purdy	Northeast Purdy	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	78
Texas	Marmaton	Hansford Marmaton	Hansford Marmaton	10 to 15	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	79
Texas	Yates	North Ward Estes	North Ward Estes	5 to 10	10 to 15	1 to 5	10 to 15	10 to 15	1 to 5	80
California	Stevens MMB	Elk Hills	Elk Hills MMB	10 to 20	10 to 15	5 to 10	20 to 30	10 to 15	5 to 10	81

**Table 7. - Tensleep, Mesaverde Almond, Weber, Sprayberry (Fractured Sandstone)**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
Wyoming	Tensleep	Wertz	Wertz	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	82
Wyoming	Tensleep	Lost Soldier	Lost Soldier	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	83 thru 86
Wyoming	Mesaverde Almond	Patrick Draw Monell	Patrick Draw Monell	5 to 10	10 to 15	5 to 10	10 to 15	10 to 15	5 to 10	
Colorado	Weber SS	Rangely	Rangely Weber Unit	5 to 10	5 to 10	1 to 5	10 to 15	5 to 10	1 to 5	87 thru 92
Texas	Sprayberry	Sprayberry	Sprayberry	0 to 2	10 to 15	5 to 10	0 to 2	10 to 15	5 to 10	93,94

**Table 8. - Heavy Oil**

State	Formation	Field	Lease	Current Economic			Life beyond 80% HCPV Inj			Bibliography References
				Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	Tertiary Recovery (%OOIP)	Gross CO <sub>2</sub> Utilization (MSCF/STB)	Net CO <sub>2</sub> Utilization (MSCF/STB)	
California	Ranger	Wilmington (Onshore)	FB1, FB3, FB5	10 to 15	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	95 thru 98
Arkansas	Ozan (Meaken Sand)	Lick Creek	Lick Creek Unit	10 to 15	15 to 20	5 to 10	10 to 15	15 to 20	5 to 10	99, 100

## Conclusion

With more than forty-five years of successful enhanced oil recovery (EOR) projects in the Permian Basin (Texas), Mississippi, Wyoming, Colorado, California, Oklahoma, and several countries worldwide, carbon dioxide CO<sub>2</sub> flooding is a proven method for extending field life. CO<sub>2</sub> acts as a solvent to overcome forces that trap oil in tiny rock pores, helping sweep immobile oil left after primary or secondary recovery operations. Generally, CO<sub>2</sub> is not miscible at first contact with reservoir oils, but miscibility can be developed in reservoirs above or near the Minimum Miscibility Pressure (MMP). CO<sub>2</sub> can attain miscibility through a multiple-contact process that vaporizes or extracts both intermediate and higher molecular weight hydrocarbons from the reservoir oil. The CO<sub>2</sub> phase picks up many intermediate hydrocarbon components from the oil, swells the oil, and reduces oil viscosity, making it mobile to move through the rock.

Advances in technology and reservoir understanding have made detailed evaluation of potential EOR candidates obtainable within months, not years. In addition, improved reservoir management and innovative investment plans have significantly reduced risks and increased rewards. Many of the original questions about CO<sub>2</sub> flooding involved the displacement efficiency of the process, how CO<sub>2</sub> would interact with the oil, and how much oil could be recovered. Many of these questions have been answered with better reservoir management tools. Not all fields are good candidates for CO<sub>2</sub> Tertiary Recovery. A reservoir must contain certain characteristics for a CO<sub>2</sub> flood to be successful. In the past, it was thought the oil must be found at depths sufficient to allow for high pressures, so that CO<sub>2</sub> and oil develop total miscibility. This is not necessary correct. Most CO<sub>2</sub> floods operate at reservoir pressures that are above their minimum miscibility pressure. But today, it is not uncommon to find CO<sub>2</sub> projects that operate below or near the minimum miscibility pressure. The CO<sub>2</sub> still produces tertiary oil. The process is not as efficient as that operated above the minimum miscibility pressure. Most historical CO<sub>2</sub> floods have targeted reservoirs that have a gravity of 25 API units or greater, but low API Gravity reservoirs are also targets. For example: Wilmington field in California produces a 14 API Gravity crude from the Ranger formation. Three pilots were conducted in Fault Blocks I, III, and V. Eventhough economic performance was reported poor, mostly due to an inadequate



CO<sub>2</sub> source and low oil price environment, a good number of wells increased oil rate from 30 BOPD to over 300 BOPD after CO<sub>2</sub> was injected. CO<sub>2</sub> has the ability to affect the full C<sub>2</sub> through C<sub>30+</sub> compositional range. Whereas, Nitrogen, and in some cases flue gas injection, will only extract the lighter components (C<sub>2</sub> through C<sub>6</sub>). In addition, a high percentage of intermediate hydrocarbons in the oil composition can be beneficial in making the overall recovery process more efficient. If these occur naturally in the oil, then the oil will probably contain a low value of Minimum Miscibility Pressure (MMP). If the oil has a high MMP, then additions such as propane, butane, condensate, or other types of hydrocarbons can be added to the CO<sub>2</sub> injection stream to lower the minimum miscibility pressure and improve overall oil recovery.

## References

### Conventional WAG CO<sub>2</sub> Flood History

1. Turek, E.A., Christopher, C.A., Stein, M.H., Merchant, D.H., "History of WAG Development" by Turek, Prepared for BP under Amoco's Learning Program, Internal Report, October, 2000.
2. Merchant, D.H., "GWR and Slug Size Optimization of the WAG Process", Prepared for Amoco Production Company, Permian Basin Business Unit, Internal Report, File: JWA-539.41-111, Model Study 1986-1987, Report Published: January 1988.
3. Merchant, D.H., "Injection Well Profiling of the CO<sub>2</sub> Recovery Process", Prepared for Amoco Production Company, Permian Basin Business Unit, Internal Report, File: DDF-539.41-1586, Model Study 1987-1988, Report Published: August 1988.
4. Merchant, D.H., "EOR/ CO<sub>2</sub> Storage Optimization and Economics 2004 CCP Program ", Prepared for BP Alternative Energy under the Carbon and Capture Program CCP, An Integrated, Collaborative Technology Development Project for Next Generation CO<sub>2</sub> Separation, Capture and Geologic Sequestration, Subcontract C010: EOR/CO<sub>2</sub> Storage Optimization and Economics – 2004 Program, Date Published: December 2004.
5. Merchant, D.H., "Enhanced Oil Recovery Methods – Conventional CO<sub>2</sub> WAG Injection", Prepared for BP Alternative Energy under the Carbon and Capture Program CCPI, An Integrated, Collaborative Technology Development Project for Next Generation CO<sub>2</sub> Separation, Capture and Geologic Sequestration, Subcontract C010: EOR/CO<sub>2</sub> Storage Optimization and Economics – 2004 Program, Date Published: October 2005.
6. Merchant, D.H., "Comparisons of Conventional CO<sub>2</sub> WAG Injection Techniques used in the Permian Basin", presented at the 15<sup>th</sup> Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, and December 10-11, 2009.
7. Tanner, C.S., Baxley, P.T., CHI, J.G., and Miller W.C., "Production Performance of the Wasson Denver Unit CO<sub>2</sub> Flood," SPE 24156, SPE/DOE Eighth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 1992.
8. Kittridge, M.G., "Quantitative CO<sub>2</sub> Monitoring, Denver Unit, Wasson (San Andres field), SPE 24644, presented at the 67<sup>th</sup> Annual Technical Conference and Exhibition of SPE held in Washington DC, October, 1992.
9. Hsu, C-F, Morell, J.I., Falls, A.H., "Field-Scale CO<sub>2</sub> Flood Simulations and Their Impact on the Performance of the Wasson Denver Unit", SPE 29116, presented at 13<sup>th</sup> SPE Symposium on Reservoir Simulation held in San Antonio, Texas, 12-15 February 1995.
10. Coalmer, M.S., Hsu, C.F., Cooper, J.C., Ward, J.B., Voto, J.G., Way, K.F., and Valdez, R., "Reservoir Characterization and Development Plan of the Wasson San Andres Denver Unit Gas Cap", SPE 56549-MS, presented at the Annual Technical Conference and Exhibition of SPE held in Houston, Texas, October 3-6, 1999.
11. Koperna, G.J., Melzer, L.S., Kuuskraa, V.A., "Recovery of Oil Resources From the Residual and Transitional Oil Zones of the Permian Basin", SPE 102972-MS, presented at the Annual Technical Conference and Exhibition of SPE held in San Antonio, Texas, September 24-27, 2006.
12. Bullock, G.W., Wood, T.B, Konecki, M.L., "A Brief History of the Wasson EOR Project", Wasson ODC, SPE 17754-PA, SPE Production Engineering Journal, Volume 5, Number 3, Pages 338-344, August, 1990.
13. Todd, M.R., Cobb, W.M., McCarter, E.D., "CO<sub>2</sub> Flood Performance Evaluation for the Cornell Unit, Wasson San Andres Field", SPE 10292-PA, Journal of Petroleum Technology, Volume 34, Number 10, Pages 2271-2282, October 1982.
14. Hsu, C-F, Fitzgerald, M.A., Musallam, S.C., McCray, T.L., Purvis, W.D., "Design and Implementation of a Grass-Roots CO<sub>2</sub> Project for the Bennett Ranch Unit", SPE 35188, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 27-29, 1996.
15. Altura Company, "Wasson Field, Bennett Ranch Unit, Wasson ODC Unit, and Denver Unit CO<sub>2</sub> Performance Update, Yoakum and Gaines County, Texas", presented at the Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 7-8, 1999.
16. Johnston, J.W., "A Review of the Willard (San Andres) Unit CO<sub>2</sub> Injection Project", SPE 6388-MS, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 10-11, 1977.
17. Wang, F.P., Lucia, F.J., Kerans, C., "Integrated Reservoir Characterization Study of a Carbonate Ramp Reservoir: Seminole San Andres Unit, Gaines County, Texas", SPE 36515-PA, SPE Reservoir Evaluation and Engineering Journal, Volume 1, Number 2, Pages 105-113, April 1998.

18. Melzer, L.S., Koperna, G.J., Kuuskraa, V.A., "The Origin and Resource Potential of Residual Oil Zones", SPE 102964-MS, presented at the Annual Technical Conference and Exhibition of SPE held in San Antonio, Texas, September 24-27, 2006.
19. Rowe, H.G., York, S.D., and Ader, J.C., "Slaughter Estate Unit Tertiary Pilot Performance", SPE 9796, presented at the 1981 SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 5-8, 1981.
20. Ader, J.C. and Stein, M.H., "Slaughter Estate Unit Tertiary Miscible Gas Pilot Reservoir Description," SPE 10727, Oil and Gas Journal, May, 1984.
21. Stein, M.H., Frey, D.D., Walker, R.D., and Pariani G.J., "Slaughter Estate Unit CO<sub>2</sub> Flood: Comparison between Pilot and Field-Scale Performance", SPE 13975, JPT, September, 1992.
22. Pariani, G. J., McCofloch, K. A., Warden, SJ., and Edens, D.R., "An Approach To Optimize Economics in a West Texas CO<sub>2</sub> Flood," JPT, Sept., 1992.
23. Merchant D.H. and Thakur, S.C., "Reservoir Management in Tertiary CO<sub>2</sub> Floods", SPE 26624, presented at the 68<sup>th</sup> Annual Technical Conference and Exhibition, Houston, Texas, October 1994.
24. Drennon, M.D., Kelm, C.H., and Whittington, H.M., "A Method for Appraising the Feasibility of Field-Scale CO<sub>2</sub> Miscible Flooding," SPE 9323, 1980 SPE Annual Technical Conference and Exhibition, Dallas, Sept 21-24, 1980.
25. Honnert, M., Creel, P., Tate, R., and Everett, D., "Five Years of Ongoing Conformance Work in the Central Mallet Unit CO<sub>2</sub> Flood in West Texas Yields Improved Economics for Operator", SPE 101701-MS, presented at First International Oil Conference and Exhibition in Mexico, August 31<sup>st</sup> to September 2<sup>nd</sup>, 2006.
26. Guillot, S.N., "Horizontal Well Applications in a Miscible CO<sub>2</sub> Flood, Sundown Slaughter Estate Unit, Hockley County, Texas", SPE 30742, SPE Annual Technical Conference and Exhibition, Dallas, October 22-25, 1995.
27. Folger, L.K., "Improved CO<sub>2</sub> Flood Predictions Using 3D Geologic Description and Simulation on the Sundown Slaughter Unit", SPE 35410, presented at SPE/DOE Tenth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 21-24, 1996.
28. Folger, L.K., Guillot, S.N., "A Case Study of the Development of the Sundown Slaughter Unit CO<sub>2</sub> Flood Hockley County, Texas", SPE 35189, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 27-29, 1996.
29. Kuo, M.C.T., Dulaney, J.P, Deer, M.W., Evans, B.S., Granquist, M.R., "Optimization of Waterflood Performance and CO<sub>2</sub> Flood Design Using a Modelling Approach, Mallet Unit, Slaughter Field", SPE 20377, presented at the 65<sup>th</sup> Annual Technical Conference and Exhibition held in New Orleans, LA, September 23-26, 1990.
30. Henry, R.L., Feather, G.L., Smith, L.R., Fussell, D.D., "Utilization of Composition Observation Wells in a West Texas CO<sub>2</sub> Pilot Flood", Levelland Unit, SPE 9786-MS, presented at SPE/DOE Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 5-8, 1981.
31. Yellig, W., "Carbon Dioxide Displacement of a West Texas Reservoir Oil", Levelland, SPE 9785-PA, SPE Oil and Gas Journal, Volume 22, Number 6, Pages 805-815, December, 1982.
32. Macon, R.B., "Design and Operation of the Levelland Unit CO<sub>2</sub> Injection Facility", SPE 8410-MS, presented at the Annual Technical Conference and Exhibition held in Las Vegas, Nevada, September 23-26, 1979.
33. Magruder, J.B., Stiles, L.H. and Yelverton, T.D., "A Review of the Means San Andres Full-Scale CO<sub>2</sub> Tertiary Project", SPE/DOE 17349, presented at the SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 17-20, 1988.
34. Hambly, E., "Means San Andres Unit – A History of CO<sub>2</sub> Flood Performance and Management", presented at the Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 7-8, 1999.
35. Jasek, D.E., Frank, J.R., Smith, D.J., "Goldsmith San Andres Unit CO<sub>2</sub> Pilot – Design, Implementation, and Early Performance", SPE 48945-MS, presented at the Annual Technical Conference and Exhibition held in New Orleans, LA, September 27-30, 1998.
36. Merchant, D.H., "Goldsmith Unit – Tertiary Performance Evaluation – CO<sub>2</sub> Prediction", developed for Shell CO<sub>2</sub> Company and Chevron USA, Internal Report, January, 2000.
37. Merritt, M.B. and Groce, J.F., "A Case History of the Hanford San Andres Miscible CO<sub>2</sub> Project", SPE/DOE 20229, presented at the SPE/DOE Seventh Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 22-25, 1990.
38. Brownlee, M.H. and Sugg, L.A., "East Vacuum Grayburg-San Andres Unit CO<sub>2</sub> Injection Project Development and Results to Date", SPE 16721, presented at the 62<sup>nd</sup> Annual Technical Conference and Exhibition, Dallas, Texas, Sept 27-30, 1987.
39. Martin, F.D. and J.E. Stevens, Harpole, K.J., "CO<sub>2</sub>-Foam Field Test at East Vacuum Grayburg/San Andres Unit", SPE 27786, presented at the SPE/DOE Tenth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 17-20, 1995.
40. Boomer, R.J., "Central Vacuum Unit CO<sub>2</sub> Performance Overview (SE New Mexico)", presented at the Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 7-8, 2001.

41. Pittaway, K.R., Albright, J.C. and Hoover, J.W., "The Maljamar Carbon Dioxide Pilot: Review and Results", SPE/DOE 14940, presented at the SPE/DOE Fifth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 20-23, 1986.
42. Moore, J.S. and Clark, G.C., "History Match of the Maljamar CO<sub>2</sub> Pilot Performance", SPE/DOE 17323, presented at the SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 17-20, 1988.
43. Roper, M.K., Cheng, C.T., Varnon, J.E., Pope, G.A. Sepehmooi, K., "Interpretation of a CO<sub>2</sub> WAG Injectivity Test in the San Andres Formation Using a Compositional Simulator", Mabee Field, SPE 24163-MS, presented at the SPE/DOE Seventh Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 22-24, 1992.
44. Jaramillo, A.R., "Utilization of a Black-Oil Simulator as a Monitor of Waterlood Operations in a San Andres Reservoir", SPE 19046-MS, GMK Unit, Unsolicited, This document was submitted for consideration for publication but included in SPE library, 1989.
45. Taylor, A.R. Hinterlong, G.H., Kumar, K.H., "West Welch CO<sub>2</sub> Flood Simulation with an Equation of State and Mixed Wettability", SPE 39808, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 23-26, 1998.
46. Keeling, R.J., "CO<sub>2</sub> Miscible Flooding Evaluation of the South Welch Unit, Welch San Andres Field", SPE/DOE 12664, presented at the SPE/DOE Fouth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 15-18, 1984.
47. Hallenbeck, L.D., Harpole, K.J., Sistrunk, G.T., and Wier, D.R., "Innovative Approach to CO<sub>2</sub> Project Development Holds Promise for Improving CO<sub>2</sub> Flood Economics in Smaller Fields Nearing Abandonment ", South Cowden Field Example, SPE 28334, presented at the 69<sup>th</sup> Annual Technical Conference and Exhibition held in New Orleans, LA, September 25-28, 1994.
48. Wegener, D.C., Harpole, K.J., "Determination of Relative Permeability and Trapped Gas Saturation for Predictions of WAG Performance in the South Cowden CO<sub>2</sub> Flood", SPE/DOE 35429, presented at the SPE/DOE Tenth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 21-24, 1996.
49. Oxy Permian, "Anton Irish Clearfork CO<sub>2</sub> Flood Case History" presented at the Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 7-8, 1999.
50. Burbank, D.E., "Early CO<sub>2</sub> Flood Experience at the South Wasson Clearfork Unit", SPE/DOE 24160, presented at the SPE/DOE Eighth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 22-24, 1992.
51. Poole, E.S. "Evaluation and Implementation of CO<sub>2</sub> Injection at the Dollarhide Devonian Unit", SPE 1722, presented at the SPE Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 1988.
52. Poole, E.S., "Evaluation and Implementation of CO<sub>2</sub> Injection at the Dollarhide Devonian Unit", SPE 17277, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 10-11, 1988.
53. Lin, E.C., Poole, E.S., "Numerical Evaluation of Single-Slug, WAG, and Hybrid CO<sub>2</sub> Injection Processes, Dollarhide Devonian Unit, Andrews County Texas", SPE 20098, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 1990.
54. Bellavance, J.F.R., "Dollarhide Devonian CO<sub>2</sub> Flood: Project Performance Review 10 years later", SPE 35190, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 27-29, 1996.
55. Kovarik, J.J., Prasad, R.K., and Waddell, Wade, and Watts, "North Dollarhide (Devonian) Unit: Reservoir Characterization and CO<sub>2</sub> Feasibility Study", SPE 27678, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 1994.
56. Pontius, S.B. and Tham, M.J., "North Cross (Devonian) Unit CO<sub>2</sub> Flood – Review of Flood Performance and Numerical Simulation Model", Journal of Petroleum Technology (December 1988), pp 1706-1714.
57. Mizenko, G.J., "North Cross (Devonian) Unit CO<sub>2</sub> Flood: Status Report", SPE/DOE 24210, presented at the SPE/DOE Eighth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 22-24, 1992.
58. Crameik, T.D., Plassey, J.A., "Carbon Dioxide Injection Project Sacroc Unit, Scurry County, Texas", SPE 72-D001, presented at the Annual Meeting Papers, Division of Production, Houston, Texas, March 6-8, 1972.
59. Graue, D.J., Blevins, T.R., "Sacroc Tertiary CO<sub>2</sub> Pilot Project", SPE 7090-MS, presented at the SPE Symposium on Improved Methods of Recovery, Tulsa, Oklahoma, April 16-17, 1978.
60. Kane, A.V., "Performance Review of a Large-Scale CO<sub>2</sub>-WAG Enhanced Recovery Project, Sacroc Kelly-Snyder Field," SPE 7091-PA, Journal of Petroleum Technology, Volume 31, Number 2, Pages 217-231, February 1979.
61. Gill, T.E., "Ten Years of Handling CO<sub>2</sub> for Sacroc Unit", SPE 11162-MS, presented at the Annual Technical Conference and Exhibition of Society of Petroleum Engineers, New Orleans, LA, September 26-29, 1982.
62. Langston, M.V., Hoadley, S.F., Young, D.N., "Definitive CO<sub>2</sub> Flooding Response in the Sacroc Unit", SPE 17321-MS, presented at the SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 17-20, 1988.
63. Hawkins, J.T., Benvegna, A.J., Wingate, T.P., McKameie, J.D., Pickard, C.D., Altum, J.T., "Sacroc Unit CO<sub>2</sub> Flood: Multidisciplinary Team Improves Reservoir Management and Decreases Operating Costs", SPE Reservoir Engineering, August 1996.
64. Bayat, M.G., Pickard, C.D., Benvegna, A.J., Wingate, T.P., Larkin, R., "Linking Reservoir Characteristics and Recovery Processes at Sacroc", Second Annual Subsurface Fluid Control Symposium, Houston, Texas, September, 1996.



65. Gonzalez, R., Schepers, K., Reeves, S., Eslinger, E., Back, T., "Integrated Clustering/Geostatistical/Evolutionary Strategies Approach for 3D Reservoir Characterization and Assisted History Matching in a Complex Carbonate Reservoir, Sacroc Unit, Permian Basin", SPE 113978-MS, presented at the SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 20-23, 2008.
66. Genetti, D.B., Whitaker, C.A., Smith, D.P., Price, L.M., "Applying Improved Recovery Processes and Effective Reservoir Management to Maximize Oil Recovery at Salt Creek", SPE 81458-MS, presented at the Middle East Oil Show, Bahrain, June 9-12, 2003.
67. Bishop, D.L., Williams, M.E., Gardner, S.E., Smith, D.P., Cochrane, T.C., "Vertical Conformance in a Mature Carbonate CO<sub>2</sub> Flood: Salt Creek Field Unit, Texas", SPE 88720-MS, presented at the Abu Dhabi International Conference and Exhibition, Abu Dhabi, United Arab Emirates, October 10-13, 2004.
68. Brinkman, F.P., Kane, T.V., McCullough, R.R., Miertschin, J.W., "Use of Full-Field Simulation to Design a Miscible CO<sub>2</sub> Flood", Sharon Ridge Field, SPE 56882-PA, SPE Reservoir Evaluation and Engineering Journal, Volume 2, Number 3, pages 230-237, June, 1999.
69. Brown, G., Carvalho, B., Wray, A., Sensa, Smith, D., Tooms, M., Pennell, S., "Monitoring Alternating CO<sub>2</sub> and Water Injection and its Effect on Production in a Carbonate Reservoir using Permanent Fiber-Optic Distributed Temperature Systems", Cogdell Field, SPE 90248-MS, presented at the Annual Technical Conference and Exhibition of Society of Petroleum Engineers, Houston, Texas, September 26-29, 2004.
70. Smith, D. and Kelly, T., "Katz (Strawn) Field CO<sub>2</sub> Project – Permian Basin, Texas", presented at the 15<sup>th</sup> Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 10-11, 2009.
71. Roy, M.B., Tucker, C.W., Lakey, C.J., Cloud, W.B., "Waterflood Redevelopment Prior to Future Tertiary Attempts – A Case History", SPE 8460 MS, Postle, presented at the SPE Oklahoma City Regional Meeting, Oklahoma City, Oklahoma, February 21-22, 1977.
72. Wehner, S.C., "A CO<sub>2</sub> EOR Update from "No Man's Land", Challenges and Successes – Postle Field, Oklahoma", presented at the 15<sup>th</sup> Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December, 10-11, 2009.
73. Kirpatrick, R.K., Flanders, W.A., and Depauw, R.M., "Performance of the Twofreds CO<sub>2</sub> Injection Project", SPE 14439, presented at the SPE/DOE Fourth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 15-18, 1984.
74. Flanders, W.A., and Depauw, R.M., "Update Case History: Performance of the Twofreds Tertiary CO<sub>2</sub> Project", SPE 26614-MS, presented at the Annual Technical Conference and Exhibition of Society of Petroleum Engineers, Houston, Texas, October 3-6, 1993.
75. Flanders, W.A., and McGinnis, R.A., "CO<sub>2</sub> EOR Economics for Small-to-Medium-Size Fields", SPE 26391-MS, presented at the Annual Technical Conference and Exhibition of Society of Petroleum Engineers, Houston, Texas, October 3-6, 1993.
76. Pittaway, K.R. and Runyan, E.E., "The Ford Geraldine Unit CO<sub>2</sub> Flood: Operating History", SPE 17278, presented at the SPE Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 10-11, 1988.
77. Phillips, J.L., McPherson, J.L., and Leibrecht, R.J., "CO<sub>2</sub> Flood: Design and Initial Operations, Ford Jeraldine (Delaware Sand) Unit", SPE 12197, presented at the 58<sup>th</sup> Annual Technical Conference and Exhibition held in San Francisco, CA, October 5-8, 1983.
78. Fox, M.J., Simlote, V.N., Stark, K.L., and Brinlee, L.D., "Review of CO<sub>2</sub> Flood, Springer "A" Sand, NE Purdy Unit", SPE/DOE 14938, presented at the SPE/DOE Fifth Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 20-23, 1986.
79. Flanders, W.A., Stanberry, W.A., and Martinez, M., "Review of CO<sub>2</sub> Performance of the Hansford Marmaton Unit", SPE/DOE 12327, presented at the SPE/DOE Enhanced Oil Recovery Symposium, Tulsa, Oklahoma, April 17-20, 1988.
80. Ring, J.N., "An Overview of the North Ward Estes CO<sub>2</sub> Flood", SPE 30729, presented at the SPE Annual Technical Conference and Exhibition, Dallas, Texas, October 22-25, 1995.
81. Oxy Elk Hills,"Enhanced Recovery from Mature Fields - An Operators Perspective", presented at RPSEA Problem Identification Forum, University of California – School of Engineering, November 29, 2006.
82. Kleinstieber, S.W., "The Wertz Tensleep CO<sub>2</sub> Flood: A Review of the Engineering Design and Initial Performance", SPE 18067, presented at the 63<sup>rd</sup> Annual Technical Conference and Exhibition of Society of Petroleum Engineers, Houston, Texas, October 2-5, 1988.
83. Brokmeyer, R.J. and Borling, D.C., "Lost Soldier Tensleep CO<sub>2</sub> Tertiary Project – Performance Case History – Bairoil, Wyoming", SPE 35191, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 27-29, 1996.
84. Merit Energy Company, "Baroil Operations Center – CO<sub>2</sub> Tertiary Recovery Review Lost Soldier and Wertz Fields, Sweetwater and Carbon County, Wyoming", Fourth Annual Wyoming Natural Gas Fair, September 28, 2000.
85. Eves, K.E. and Nevarez, J.J., "Update of Lost Soldier/Wertz Floods – Living in a Constrained CO<sub>2</sub> Environment", presented at the 15<sup>th</sup> Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 10-11, 2009.

86. Kulkarni, M. M., Chen, Hung-Lung, Brummert, A.C., "CO<sub>2</sub> IOR Evaluation for the U.S. Rocky Mountain Assets", SPE 113297-MS, presented at the SPE/DOE Symposium on Enhanced Oil Recovery, Tulsa, Oklahoma, April 20-23, 2008.
87. Larson, W.K., "Rangeley Weber Sand CO<sub>2</sub> Project: A Case History", presented at the Denver SPE MiniSymposium, November 19, 1987.
88. Wackowski, R.K., Stevens, C.E., Masoner, L.O., Attanucci, V., Larson, J.L., Aslesen, K.S., "Applying a Rigorous Decision Analysis Methodology to Optimization of a Tertiary Recovery Project: Rangely Weber Sand Unit, Colorado", SPE Oil and Gas Economics, Finance, and Management Conference held in London, England, 28-29, April 1992.
89. Wakowski, R.K. and Masoner, L.O., "Rangely Weber Sand Unit CO<sub>2</sub> Project Update: Operating History", SPE/DOE 27755, presented at the SPE/DOE Ninth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 17-20, 1994.
90. Fulbright, G.D, Hild, G.P., Horf, T.A., Myers, F.S., O'Toole, F.S., Wakowski, R.K., "Evolution of Conformance Improvement Efforts in a Major CO<sub>2</sub> WAG Injection Project, Rangly Field, Colorado", SPE/DOE 35361, presented at SPE/DOE Tenth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 21-24, 1996.
91. Masoner, L.O., Abidi, H.R., Hild, G.P., "Diagnosing CO<sub>2</sub> Flood Performance Using Actual Performance Data", Rangely Field – Colorado, SPE/DOE 35363, presented at SPE/DOE Tenth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 21-24, 1996.
92. Wackowski, R.K., "Rangely Weber Sand Unit CO<sub>2</sub> Project Update", Powerpnt talk presented at the 5<sup>th</sup> Annual CO<sub>2</sub> Flooding Conference, Midland, Texas, December 10-11, 1999.
93. Schechter, D.S., McDonald, P., Sheffield, T., Baker, R. "Integration of Laboratory and Field Data for Development of a CO<sub>2</sub> Pilot in the Naturally Fractured Spraberry Trend Area, Permian Basin, Texas", SPE 36657, presented at the Annual Technical Conference and Exhibition held in Denver, CO., October 6-9, 1996.
94. Schechter, D.S., McDonald, P., Sheffield, T., Baker, R. "Reservoir Characterization and CO<sub>2</sub> Pilot Design in the Naturally Fractured Spraberry Trend Area, Permian Basin, Texas", SPE 35469, presented at the Permian Basin Oil and Gas Recovery Conference, Midland, Texas, March 27-29, 1996.
95. Spivak, A., Garrison, W.H., Nguyen, J.P., "Review of an Immiscible CO<sub>2</sub> Project, Tar Zone, Fault Block V, Wilmington Field, California", SPE 17407-PA, SPE Reservoir Engineering Journal, Volume 5, Number 2, Pages 155-162, May, 1990.
96. Saner, W.B., Patton, J.T., "CO<sub>2</sub> Recovery of Heavy Oil: Field Test", SPE 12082, presented at the Annual Technical Conference and Exhibition held in San Francisco, California, October 5-8, 1983.
97. Sankur, V., Creek, J.L., DiJutio, S.S, Emanuel, A.S., "A Laboratory Study of Wilmington Tar Zone CO<sub>2</sub> Injection Project", SPE 12751, presented at the California Regional Meeting held at Long Beach, California, Apr 17-23, 1984.
98. Jeschke, P.A., Schoeling, L., Hemmings, J., "CO<sub>2</sub> Flood Potential of California Oil Reservoirs and Possible CO<sub>2</sub> Sources", SPE 63305, presented at the SPE/AAPG Western Regional Meeting held in Long Beach, California, June 19-23, 2000.
99. Reid, T.B., Robinson, H.J., "Lick Creek Meakin Sand Unit Immiscible CO<sub>2</sub>/Waterflood Project", SPE 9795, presented at SPE/DOE Tenth Symposium on Improved Oil Recovery, Tulsa, Oklahoma, April 6-7, 1981.
100. Moffitt P.D., Zornes, D.R., "Lick Creek Meakin Sand Unit Immiscible CO<sub>2</sub>/Waterflood Project", presented at the 67<sup>th</sup> Annual Technical Conference and Exhibition held in Washington DC, October 4-7, 1992.
101. Brock, W.R. and Bryan, L.A.: "Summary Results of CO<sub>2</sub> EOR Field Tests, 1972-1987," paper SPE 18977 presented at the 1989 SPE Joint Rocky Mountain Regional/Low Permeability Reservoir Symposium and Exehibition, Denver, 6-8 March, 1989
102. Caudle, B.H. and Dyes, A.B.: "Improving Miscible Displacement by Gas-Water Injection" Trans., AIME (1958) 213, 281.
103. Hadlow, R.E.: "Update of Industry Experience with CO<sub>2</sub> Injection," paper SPE 24928 presented at the 1992 SPE Annual Technical Conference and Exhibition, Washington, DC, 4-7 October.
104. Grigg, R.B. and Schechter, D.S.: "State of the Industry in CO<sub>2</sub> Floods," paper SPE 38849 presented at the 1997 SPE Annual Technical Conference and Exhibition, San Antonio, Texas 5-8 October, 1997
105. John D. Rogers, \*SPE, and Reid B. Grigg, SPE, New Mexico Petroleum Recovery Reseach Center.: "A Litature Analysis of the WAG Injectivity Abnormalities in the CO<sub>2</sub> Process" SPE Report (SPE 73830) was revised for publication, first presented at 2000 SPE/DOE IOR Symposium, Tulsa Apr 3-5 2000
106. Pennzoil's Sacroc Development Team (1994-1998): Dr. Ghasem Bayat, Tony Benvegna, Claud Pickard, Jack Horkowitz, Tom Wingate, Don Hartman; Team was Responsible for Sacroc's Centerline Project plus two other pilot programs that was responsible for 1/3 of Sacroc's total 9,600 BOPD Production through this time period.
107. Amoco's Permian Basin Original Model Development Group: Jack Aulick(Manager), Reservoir Modellers: Kevin McCollough, Steve Pennell, Burt Nelson, Gary Pariani, Dennis Edens, John Kimberling, and David Merchant, Operations: Perry Jarrell; Team was responsible for developing Amoco's Tapered WAG Operating scheme.
108. Steve Melzer, Midland 2016 CO<sub>2</sub> Conference, "Plot of Historical Oil Price Crash Periods from the 1970's through 2016", Date: December 2016.

---

## Acknowledgements

I would like to express my gratitude to the members of the Carbon Management Technology Conference (CMTC) for allowing me the opportunity to be part of this CO<sub>2</sub> Conference. I would especially like to thank George Koperna of Advanced Resources International and Jose Figueroa for their support in making this effort possible.

David H. Merchant  
Merchant Consulting  
Magnolia, Texas